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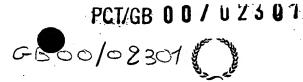
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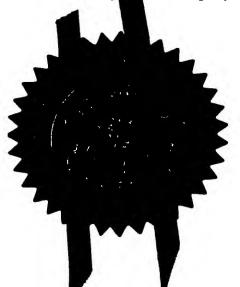
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Patents Act 1977 (Rule Request for grant of a patent P01/7700 0.00 he Patent Office (See the notes on an explanatory led Cardiff Road you fill in this form) Newport Gwent NP9 1RH Your reference BKCD/NS/DBN.104a Patent applica 9922693.8 25 SEP 1999 (The Patent Office 3. Full name, address and postcode of the or of each applicant (underline all surnames) Trikon Holdings Limited Coed Rhedyn Ringland Way Newport Patents ADP number (if you know it) Gwent NP6 2TA 43542300 If the applicant is a corporate body, give the country/state of its incorporation United Kingdom Title of the invention Method and Apparatus for Forming a film on a Substrate. Name of your agent (if you have one) Wvnne-Jones, Laine & James "Address for service" in the United Kingdom to which all correspondence should be sent 22 Rodney Road (including the postcode) Cheltenham GL50 1JJ Patents ADP number (if you know it) 1792001 6. If you are declaring priority from one or more Country Priority application number Date of filing earlier patent applications, give the country (if you know it) (day / month / year) and the date of filing of the or of each of these earlier applications and (if you know it) the or each application number 7. If this application is divided or otherwise Number of earlier application Date of filing derived from an earlier UK application, (day / montb / year) give the number and the filing date of the earlier application 8. Is a statement of inventorship and of right to grant of a patent required in support of Yes this request? (Answer 'Yes' if: a) any applicant named in part 3 is not an inventor, or b) there is an inventor who is not named as an applicant, or c) any named applicant is a corporate body.

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11.

I/We request the grant of a patent on the basis of this application.

Signature

Wynne-Jones, Laine

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24 9 99

 Name and daytime telephone number of person to contact in the United Kingdom

Mr. B. Dunlop

01242 515807

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Method and Apparatus for Forming a film on a Substrate

In our pending application No. 9914879.3, the contents of which are hereby incorporated by reference, we described a method for forming a film on a substrate comprising:

- (a) positioning the substrate on the support in a chamber;
- (b) supplying to the chamber in gaseous or vapour form a silicon containing organic compound and an oxidising agent in the presence of a plasma to deposit a film on the substrate; and
- (c) setting (e.g. by annealing) the film such that carbon-containing groups are retained therein.

We suggest that the preferred oxidising agent is oxygen and indicate that the silicon-containing organic compound may be an alkylsilane or a tetralkylsilane.

Further experiments have now been carried out which suggest that methoxysilanes and in particular methoxymethylsilanes produce films with very low dielectric constants and may be particularly preferred.

Particularly good results have been achieved with cyclohexyldimethoxymethylsilane (CHDMMS) which has the following structure:

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Experiments have also shown that a methoxysilane (e.g. CHDMMS may be able to be processed as in the above method described, but without any oxidising agent present in the plasma. It is supposed that this is because the Si-O bond already exists as part of the methoxy group.

Accordingly, according to another aspect the invention consists in a method of forming a film on a substrate comprising:

- (a) positioning the substrate on a support in a chamber;
- (b) supplying to the chamber in gaseous or vapour form an organic compound including an Si-O bond to deposit a film on the substrate; and
- (c) setting (e.g. annealing) the film such that carbon-containing groups are retained therein.

Preferably the compound is supplied in the presence of a plasma, but other energy sources may be utilised to cause appropriate deposition and these may be combined with spin-on techniques.

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As before the platen or support temperature may be low, and initial experiments as shown in Figure 6 were carried out at various temperatures from 0°C to 70°C. Subsequent experiments have been carried out with a platen temperature of 50°C rather than 0°C as previously described in British Patent Application No. 9914879.3.

The invention will be described with reference to the accompanying drawings, in which:

Figure 4 is a Fourier Transform Infra-Red (FTIR) spectrum for a first process run without oxygen; and

Figure 5 is the equivalent FTIR for the process run with oxygen;

Figure 6 is a table showing initial experimental results using standard delivery systems for CHDMMS;

Figure 7 is a table showing experimental results using a syringe pump to deliver CHDMMS; and

Figures 8 to 10 are FTIR spectrum relating to certain experiments identified in Figure 7.

An experiment has particularly been carried out using cyclohexyldrimethoxymethylsilane (CHDMMS). As is reported below this has shown significantly reduced dielectric constants. It is anticipated that benefits will be found from many methoxysilane compounds such as tetramethoxysilane.

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The experiments were carried out in chamber substantially as shown in Figure 1 of our co-pending application 9914879.3 with an electrode gap spacings of 40mm and 20mm and the uniformity ring shield used for non plasma based processes removed. The CHDMMS was fed into 5 the chamber using a syringe delivery system described in our co-pending application (filed and entitled "Delivery Liquid Precursors to Semiconductor Processing Reactors", which is incorporated herein by reference), on the same date as opposed to a traditional low vapour 10 pressure mass flow controller. This was done due to the fact that, as described below, CHDMMS could not reliably delivered by conventional means as it has a relatively high boiling point (approximately compared to most of the 15 other precursor materials investigated in application 9914879.3.

All processes were run with plasmas applied to the showerhead. All wafers were 'set' by annealing for typically 30 minutes at approximately 480°C.

The following parameter ranges have been investigated:

Pressure - 500 mT to 1500 mT

Power (380 kHz) - 50 W to 750 W

Platen temperature - 0°C to 70°C

CHDMMS flows - 0.5 g/min to 1.5 g/min

Oxygen flows - 0.40 2000 areas

Oxygen flows - 0 to 200 sccm
Nitrogen flows - 0 to 400 sccm
Peroxide flows - 0 to 0.75 g/min

It will be appreciated that the relative flow rates are particularly relevant to the process. In general higher rates lead to higher deposition rates and thus a broad range of flow rates can achieve similar results. Thus values outside the above ranges may be applicable.

Two particularly preferred process examples are given below: one of these is with oxygen and one is without oxygen.

Process 1 (no 02)	
Pressure	900 mT
Power	500 W
Platen temperature	50°C
CHDMMS flow	0.85 g/min
Nitrogen flow	200 sccm

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Process 2 (with 0_2)	
Pressure	900 mT
Power	250 W
Platen temperature	50°C
CHDMMS flow	0.85 g/min
Oxygen flow	50 sccm
Nitrogen flow	150 sccm

The resultant films were annealed and the post anneal results were as follows:

Process 1 (no 0_2)	
Deposition rate	17000Å/min
Uniformity (max/min)	± 4%
Refractive index	1.370
Dielectric constant	2.55

Process 2 (with 02)	
Deposition rate	9500Å/min
Uniformity (max/min)	± 5%
Refractive index	1.340
Dielectric constant	2.25

As can be seen the dielectric constants in each case are desirably low, but the "with oxygen" process is significantly advantageous.

Figures 4 and 5 show the respective FTIR spectra. It will be seen that they are substantially similar. The feature between 2500 and 2000 in Figure 5 is believed to result from atmospheric (background) CO_2 .

In fact, initial experiments were carried out using a CHMMS source consisting of a PTFE pot within an evacuated aluminium vessel which was heated to 150° C. The pot was connected by gas line to a gas mass flow controller suitable for H_2O with a conversion factor of 1.000. The RF power was applied to the showerhead with a spacing from the wafer of 40mm. The RF was $380 \, \text{khz}$ continuous mode. Results from these experiments are shown in Figure 6. The

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numbers in the CHMMS column are the nominal gas flow as measured by the mass flow controller however stable flows could not be achieved and therefore these results are for near random quantities of CHMMS being delivered to the process chamber. At this point experimentation was halted until a superior delivery system for this precursor could be developed.

CHMMS has a boiling point of 201.2°C, and a density of 0.940 g/cc. As it was noted in these experiments that CHMMS deposits a low k insulator without the addition of an oxidising agent it is therefore possible that it could be delivered as a liquid to a semiconductor wafer without a chamber being required (e.g. by well known 'spin-on' techniques) and then reacted either thermally or by plasma to form a low k (k<3) insulator layer. The apparatus used may in effect deposit a liquid by vaporising the liquid precursor, delivering it as a vapour and then condensing it onto the wafer at a temperature below the boiling point of the precursor at that pressure. It is not yet clear if the reactions take place to the precursor on the wafer or at some other place, depositing reaction products onto the wafer.

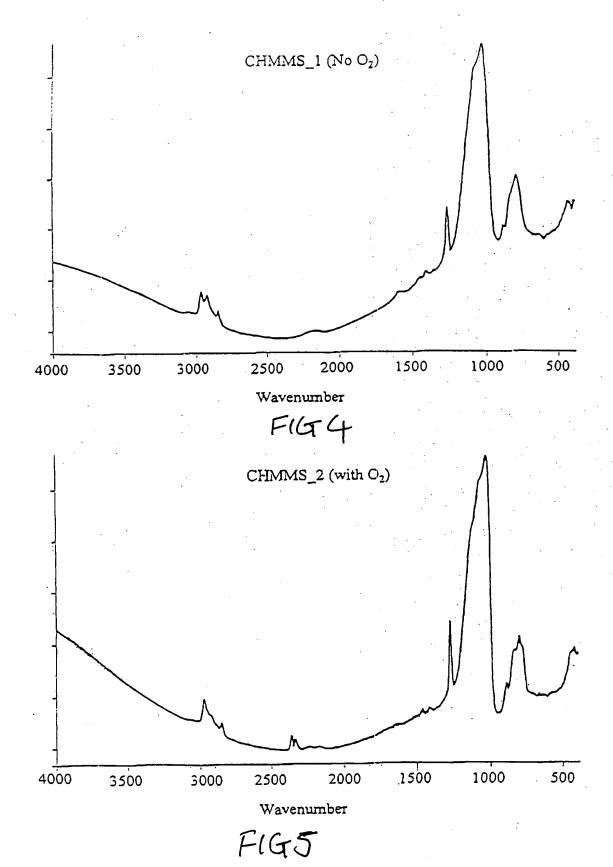
Having developed a more suitable liquid delivery system which utilises a syringe pump, further experiments

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were carried out as shown in Figure 7. From these experiments preferred processes were developed as further described here. FTIR for runs 13, 14 and 16-23 respectively are illustrated in Figures 8 to 10.



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Flowfill chamber depositions using Cyclohexyldimethoxymethylsilane

P727 - Flowfill chamber (Flow_1), 40mm el ctrode gap - Syringe delivery system

Process parameters

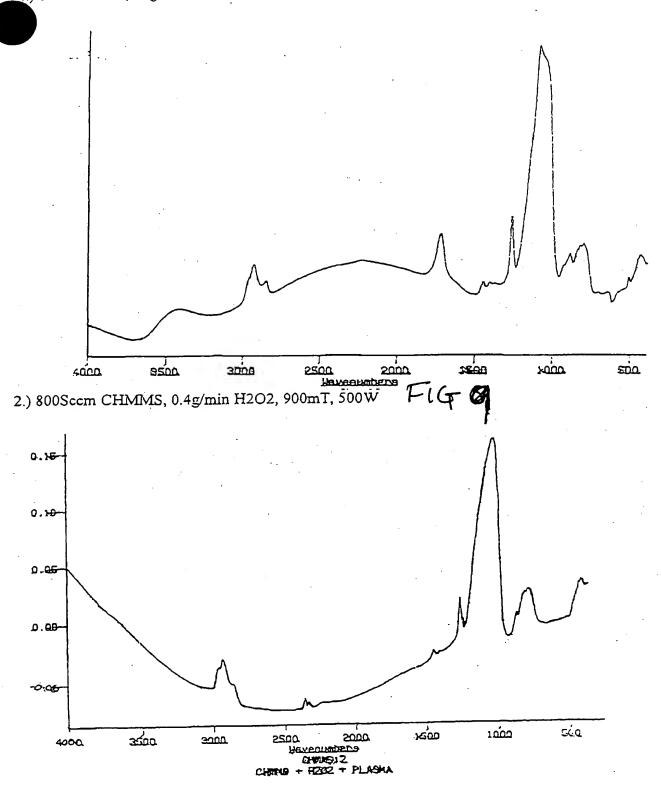
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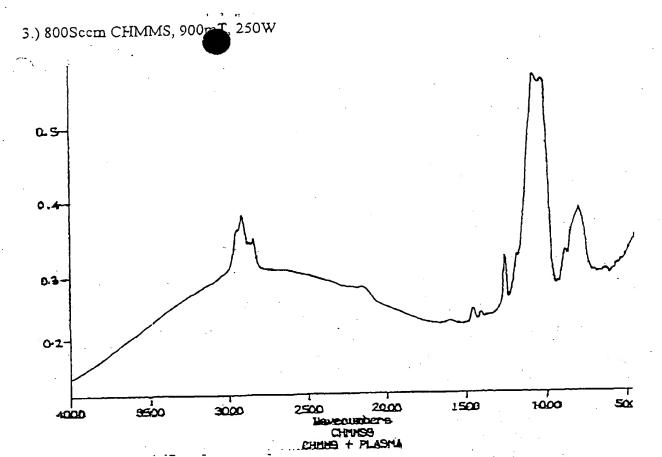
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50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 6 6 6 9 2.286 6 6 6 9 2.286 6 6 6 9 2.286 6 8 9 0.093 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.098 3 0.0143 0.0771 3 3 1.488 1.292 0.0282 0.0143 0.0771 3 0.0143 0.0771 3 1.484 1.496 0.0278 0.0143 0.0771 3 1.434 1.496 0.0278 0.0143 0.0771 3 1.344 1.344 1.344 0.0278 0.0143 0.0771 3 1.447 1.474	250	100(8)		130
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 12080 7.6 1.5107 2.286 6 50 12502 5.1 1.5081 2.28 0.0239 0.0993 0.096 3 50 12502 5.1 1.5081 2.9 0.0235 0.0119 0.0116 3 50 12607 3.5 1.4983 2.9 0.0282 0.0149 0.0912 5 50 124074 3.5 1.4986 2.72 0.0282 0.0143 0.0771 3 50 12330 2.4 1.496 2.72 0.0283 0.0143 0.0771 3 50 17626 - 1.3437 0.0238 0.0143 0.0771 3 50 17626 - 1.3437 0.0238 0.0143 0.0771 3 50 12785 8.4 1.3756 0.0233 0.0143 0.0724 50	250	125(8)	0.85 7	129
50 9888 11.7 1.4392 0.0343 0.0117 0.1441 50 50 2.286 2.286 6 50 12080 7.6 1.5107 2.426 0.0239 0.0933 0.096 3 50 12502 5.1 1.5081 2.9 0.0239 0.0933 0.096 3 50 12470 3.5 1.4983 0.0222 0.0149 0.0711 3 50 12470 3.5 1.4983 0.0228 0.0143 0.0771 3 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 3 50 17626 1.498 2.72 0.0278 0.0143 0.0771 3 50 17626 1.3437 1.3437 1.4337 1.4347 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 1.447 <td>250</td> <td>-</td> <td> </td> <td>128</td>	250	-	 	128
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 6 50 12080 7.6 1.5107 2.426 0.0239 0.0093 0.096 3 50 12502 5.1 1.5081 2.9 0.0239 0.0093 0.096 3 50 12502 5.1 1.5081 2.9 0.0232 0.0149 0.0912 3 50 12607 3.5 1.4983 2.9 0.0282 0.0149 0.0912 3 50 13930 2.4 1.498 2.9 0.0278 0.0143 0.0771 3 50 17626 - 1.3437 2.72 0.0143 0.0771 3 50 17626 - 1.3437 2.72 0.0143 0.0771 3 50 17628 1.4 1.3654 3 0.0273 0.0274 0.0274 50 12888 <t< td=""><td>250</td><td>175(8)</td><td>0.85 2</td><td>127</td></t<>	250	175(8)	0.85 2	127
SO 9848 11.7 1.4392 2.437 2.437 50 50 2.286 2.286 2.286 50 2.286 50 2.286 50 2.286 50 2.286 50 2.286 50 2.286 50 2.296 50 2.292 0.0093 0.096 50 2.292 5.1 1.5081 2.9 0.0232 0.0119 0.0116 50 50 14074 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 13930 2.4 1.496 2.72 50 13930 2.4 1.496 2.72 50 17626 50 17626 50 1.3437 50 17626 50 11436 17.6 1.3437 50 12828 13.6 1.3437 50 12828 13.6 1.3888 50 12828 13.6 1.3475 50 12828 13.6 1.3475 50 12828 13.6 1.3475 50 12828 13.6 1.3475 50 12828 13.6 1.447 50 50 12828 1.4745 50 50 12828 1.4745 50 50 12828 1.4549 50 0.0255 0.0143 0.0074 50 50 14852 2.3 1.4384 2.556 50 50 14852 2.3 1.4384 2.556 50 50 1633 1.4384 2.556 50 50 1633 1.4384 2.556 50 50 10515 1.397 0.0329 0.0069 0.0493 0.0071 0.0510 0.0515 0.0515 0.0343 0.0071 0.0526 0.0343 0.0051 0.0526 0.0343 0.0051 0.0526 0.0343 0.0051 0.0526 0.0343 0.0052 0.0343 0.0054 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051 0.0526 0.0344 0.0051	250			126
50 9888 11.7 1.4992 2.437 0.034 0.017 0.1441 5 50 50 2.280 2.287 2.426 0.0239 0.0996 6 50 12080 7.6 1.5107 2.426 0.0239 0.0996 3 50 12502 5.1 1.5081 2.9 0.0225 0.0119 0.0116 3 50 12670 5.1 1.5081 2.9 0.0225 0.0119 0.0116 3 50 14074 3.5 1.4983 2.9 0.0282 0.0149 0.0912 3 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 3 50 17626 - 1.3437 0.0278 0.0143 0.0771 3 50 117626 - 1.3437 0.0278 0.0143 0.0771 3 50 12828 13.6 1.3713 0.0278 0.0243 0.0724	250	125(8)		
50 9888 11.7 1.4992 0.0334 0.0117 0.1441 5 50 50 12080 7.6 1.5107 2.426 0.0239 0.0093 0.996 3 50 12502 5.1 1.5081 2.9 0.0239 0.0119 0.0116 3 50 14074 3.5 1.4983 2.9 0.0223 0.0119 0.0116 3 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 3 50 13930 2.4 1.496 0.0278 0.0143 0.0771 3 50 13930 2.4 1.496 2.72 0.0143 0.0771 3 50 17626 - 1.3437 0.0282 0.0143 0.0771 3 50 11436 17.6 1.3437 0.0283 0.0143 0.0721 3 1.4348 0.0225 0.0143 0.0724 0.0225 0.0143 0.0724 0.0363	250	185(8)		2
50 9848 11.7 1.4392 2.437 0.0134 0.0117 0.1441 50 50 12080 7.6 1.5107 2.286 2.286 6 50 12080 7.6 1.5107 2.426 9 0.093 0.096 6 50 12502 5.1 1.5081 2.9 0.019 0.0116 6 6 6 1.2470 0.0239 0.0093 0.096 1 6 1.2470 0.02470 0.0116 1.2483 0.0228 0.0119 0.0116 1 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0724 0.0278 0.0143 0.0724 0.0255	250	150(8)	0.85 50	123
50 9848 11.7 1.4392 0.0334 0.0117 0.1441 50 50 12080 7.6 1.5107 2.286 0.0239 0.0993 0.966 50 12502 5.1 1.5107 2.426 0.0239 0.0993 0.966 50 20470 5.1 1.5081 2.9 0.0119 0.0116 50 14074 3.5 1.4983 2.9 0.0282 0.0119 0.0116 50 14074 3.5 1.4983 2.9 0.0282 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 17628 13.6 1.3437 0.0272 0.0273 0.0771 50 12828 13.6 1.3713 0	250	175(8)	0.85 25	122
SO 988 11.7 1.4592 2.437 2.437 2.437 50 50 50 12080 7.6 1.5107 2.286 50 12502 5.1 1.5081 2.9 0.0239 0.0993 0.096 50 12502 5.1 1.5081 2.9 0.0239 0.0119 0.0116 50 13930 2.4 1.496 2.72 0.0235 0.0119 0.0116 50 13930 2.4 1.496 2.72 0.0282 0.0149 0.0912 50 17626 -	250	200(8)	0.85 0	121
\$0 9888 11.7 1.4592 0.0334 0.0117 0.1441 \$0 50	500	200(8)	0.85 0	120
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.287 0.0239 0.0093 0.096 2.096 2.287 0.0143 0.0714 2.287 0.0143 0.0771 2.287 0.0143 0.0771 2.287 0.0143 0.0771 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2.287 2	500	200(8)		119
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 0.0239 0.093 0.096 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.0239 0.093 0.096 50 14074 3.5 1.4983 2.9 0.0119 0.0116 50 13930 2.4 1.496 0.0282 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 12828 13.6 1.3888 0.0343 0.0343 0.0724 50 10020 8.6 <td>500</td> <td>200(8)</td> <td>-</td> <td>118</td>	500	200(8)	-	118
50 9848 11.7 1.4592 0.034 0.0117 0.1441 50 50 12080 7.6 1.5107 2.286 9.0093 0.096 50 12080 7.6 1.5107 0.0239 0.0093 0.096 50 12502 5.1 1.5081 0.0239 0.0093 0.096 50 14074 3.5 1.4983 0.0255 0.0119 0.0116 50 13930 2.4 1.496 2.9 0.0282 0.0149 0.0912 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 11436 1.7.6 1.3713 0.0255 0.0143 0.0714 50 12828 13.6 1.3888 0.0255 0.0143 0.0724 <td>500</td> <td>4</td> <td>+</td> <td>117</td>	500	4	+	117
50 9848 11.7 1.4592 0.034 0.0117 0.1441 50 50 2.286 2.286 2.286 90.0093 0.096 50 12080 7.6 1.5107 2.426 90.0093 0.096 50 12502 5.1 1.5081 90.023 0.0093 0.096 50 14074 3.5 1.4983 2.9 90.0119 0.0116 50 13930 2.4 1.496 9.0278 0.0149 0.0912 50 13930 2.4 1.496 9.0278 0.0143 9.0771 50 13930 2.4 1.496 2.72 9.0143 9.0771 50 17626 - 1.3437 9.0278 0.0143 9.0771 50 11436 1.3654 1.3713 9.004 9.004 1.3437 9.004 9.004 9.004 9.004 9.004 9.004 9.004 9.004 9.004 9.004 9.004 9.004	500	200(8)	+	116
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 2.286 2.286 2.286 9.0093 0.096 0.093 0.096 0.095 0.095 0.096 0.096 0.0239 0.0093 0.096 0.096 0.0239 0.0093 0.096 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0119 0.0116 0.027 0.0143 0.0771 0.027 0.0143 0.0771 0.027 0.0143 0.0771 0.0278 0.0143 0.0771 0.027 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143 0.0771 0.0278 0.0143<	500	200(8)	0.85	115
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 2.286 2.286 9.0093 0.096 50 12080 7.6 1.5107 0.0239 0.0093 0.096 50 12502 5.1 1.5081 0.025 0.0119 0.0116 50 20470 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 12828 13.6 1.3888 0.0234 0.0143 0.0771	500	200(8)	+	114
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 0.0239 0.093 0.096 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.025 0.0119 0.0116 50 20470 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 14074 3.5 1.4983 0.0228 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0143 0.0771 50 17626 - 1.3437 - - - 50 21765 8.4 1.3654 - - - - 50 12828 13.6	500	200(8)		113
50 9848 11.7 1.4392 0.034 0.0117 0.1441 50 50 2.286 2.286 0.0239 0.093 0.096 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 2.9 0.0119 0.0116 50 20470 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 CHAMBER SPACING CHANGED TO 20MM 2.72 0.0278 0.0143 0.0771 50 17626 - 1.3437 0.0278 0.0143 0.0771 50 21765 8.4 1.3654 0.0278 0.0143 0.0771 50	500	200(8)	0.85	113
50 9848 11.7 1.4392 0.0334 0.0117 0.1441 50 50 2.286 2.286 9.0093 0.096 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.025 0.0119 0.0116 50 20470 3.5 1.4983 0.0282 0.0149 0.0912 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771 CHAMBER SPACING CHANGED TO 20MM 50 21765 8.4 1.3654 1.3654 0.0143 0.0771 50 11436 17.5 1.3713 0.0278 0.0143 0.0771	250	175(8)	$\frac{1}{1}$	
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 50 2.286 2.286 9.0093 9.096 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.023 0.0119 0.0116 50 20470 2.9 0.028 0.0119 0.0116 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 50 17626 1.3437 2.72 0.0143 0.0771 50 21765 8.4 1.3654 0.034 0.0143 0.0771	250	175(8)	+	3
50 9848 11.7 1.4592 0.034 0.0117 0.1441 50 50 2.286 2.286 9 9 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.023 0.0119 0.0116 50 20470 2.9 0.028 0.0119 0.0116 50 14074 3.5 1.4983 0.0282 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 50 13930 2.4 1.496 2.72 0.0143 0.0771 60 17626 - 1.3437 1.3437 0.0278 0.0143 0.0771	500	200(8)	0 85 0	8
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 50 2.286 2.286 9 50 12080 7.6 1.5107 0.0239 0.093 0.096 50 12502 5.1 1.5081 0.025 0.0119 0.0116 50 20470 2.9 0.025 0.0119 0.0116 50 14074 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 13930 2.4 1.496 0.0278 0.0143 0.0771 CHAMBER SPACING CHANGED TO 20MM 2.72 0.0143 0.0711	500	200(8) 900	0.85 0	108
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 30 2.286 2.286 30 30 30 30 30 30 30 30 30 30 30 30 30 30 30 30 30 30 3.5 1.4983 2.9 0.0282 0.0149 0.0912 50 13930 2.4 1.496 2.72 0.0278 0.0143 0.0771			-	
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 30 2.286 2.286 30 30 30 30 3.5 3.581 3	750		0.85 0	
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 30 2.437 2.437 30 <t< td=""><td>750</td><td>'n</td><td>0.85 0</td><td>106</td></t<>	750	'n	0.85 0	106
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 50 2.286 2.286 3.286 3.286 3.286 3.286 3.286 3.2426	750		0.85 0	201
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 50 2.286 2.286 3.286	500	ā	-	104
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 2.286 2.286 2.286 3.0 3.0 2.426 3.0	500			3
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 2.437 2.286 2.286 50 2.426 2.426	500	_	+	102
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 2.437 2.437 50 2.286	250	175(8)	-	<u></u>
50 9848 11.7 1.4592 0.0334 0.0117 0.1441 50 2.437 0.034 0.0117 0.1441	250	175(8)	1	00
50 9848 11.7 1.4592 0.0334 0.0117 0.1441	250	-	0.85 25	8
60 0040 11.7 14600 00004 00117 01441	250	175(8)	-	98
50 9917 8.8 1.4521 0.0342 0.0093 0.1091	250	175(8) 900	-	97
50 2.48	250	150(8)	0.85 50	8
50 2.49	250	150(8) 900	0.85 50	95
21408 4.6 1.4199 0.0273 0.0076 0.0725	500	0	. 0.85 50	. 94

FlG7 (cential)

(1) 800CHMMS, 0.4g/min H2O2, 900mT, 250W as deposited



F148.



F1610

1-CT 1 98001 301 6700 Wynni-Jones Laines James